





Article

Energy Efficiency Analysis of Fixed-Speed Pump Drives with Various Types of Motors

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Featured Application: The presented results can be used to assess the energy-saving potential of general purpose and industrial electric motors of various types in various applications of electric drives.

Abstract: The paper presents a comparative analysis of energy consumption by 2.2 kW electric motors of various types and energy efficiency classes in the electric drive of a pump unit with throttle control in a water supply system. Line-start permanent-magnet synchronous motors of the IE4 energy efficiency class and induction motors of the IE4 and IE3 energy efficiency classes of various manufacturers were considered (IE4 and IE3 are labels of energy efficiency classes of electric motors according to IEC 60034-30-1 standard). Energy consumption at a hydraulic load changing under a typical duty cycle was calculated based on the nameplate data of the pump and electric motors. The developed method shows that selecting an electric motor based on the IE energy efficiency class under the IEC 60034-30-1 standard (i.e., based on efficiency at a rated load) may not provide the minimum energy consumption of a variable flow pump unit over a typical duty cycle. In particular, the considered IE4 class line-start permanent-magnet synchronous motors do not provide significant advantages over IE4 class induction motors, and sometimes even over IE3 class induction motors when they are used in variable flow pump units.

Keywords: centrifugal pump; energy efficiency; energy efficiency class; induction motor; line-start permanent-magnet synchronous motor; throttling control

1. Introduction

Despite the high efficiency and the high dynamic and static performance of variable speed drives (VSDs), electric motors powered directly from the mains are widely used in many applications due to the high cost of frequency converters. For instance, the market share of variable-speed drives is estimated to be about 30% in Germany according to the European Commission data [1] and about 20% in Switzerland according to the study disclosed in Phillips and Tieben [2].

In particular, such widely used machines, including centrifugal pumps, compressors, and fans, do not require a wide adjustment range, high starting torque, or high speed. Therefore, induction motors (IMs) powered directly from the mains are widely used in the drives of the above-mentioned fluid machinery. Furthermore, several manufacturers offer line-start permanent-magnet synchronous

motors (LSPMSM) of a high energy efficiency class powered directly from the mains. The adjustment of fluid flow in this case is carried out using throttle control valves.

According to the data from the International Energy Agency [3], electric motors consume 46% of the world's electricity. They account for about 70% of the total industrial electricity consumption. According to the report of the European Commission [3], pump systems consume almost 22% of all electric energy generated throughout the world, as shown in Figure 1. Therefore, it is a pressing task to study the possibilities of increasing the energy efficiency of pump units. Improvements in energy efficiency of a pump unit can be provided by implementing changes in the hydraulic network in which the unit operates by using control systems, including a variable-speed drive, by optimizing and distributing the load (when units run in parallel), as well as by proper selection of the unit parts, in particular, via the use of electric motors of a higher energy efficiency class [4]. The latter method is considered in Shankar et al. [4] as the most relevant method for pumps under throttle control.

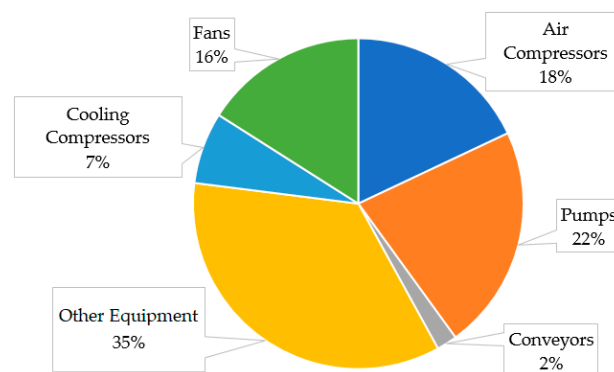


Figure 1. Energy consumption of various applications [5].

The minimum energy efficiency level for electric motors is defined in Annex I of European Commission [5]. Energy efficiency classes of line operated AC motors are determined in IEC 60034-30-1 standard [6]. In accordance with the EC regulation [5], since 1 January 2017, all electric motors with power ranging from 0.75 to 375 kW must have an energy efficiency class of at least IE3, or IE2 if they are used as part of a VSD (E4, IE3 and IE2 are labels of energy efficiency classes of electric motors according to IEC 60034-30-1 standard). Within the planned timeframe, according to Policy Option 4 [7], the introduction of the minimum acceptable energy efficiency class of at least IE4 is expected before 2030.

The classification of electric motors in References [5,6] takes into account only the motor rated efficiency specified by the rated shaft power, but not the motor efficiency at underload modes, which is of at least comparable relevance for motors used as components of pump units [8].

In practice, most of the time, the centrifugal pump is employed at low or medium loads. However, the pumps are designed and integrated to satisfy maximal load conditions [9]. Also, it is estimated in Shuvalova [10] that 75% of the centrifugal pumps are oversized, many by more than 20%. In Glover and Lukaszczyk [11], it is estimated that only 20% of the pump drive motors in operation are running at their rated mode. References [12,13] provide comparisons of energy consumption by a pump unit with electric motors of various types and IE classes with a VSD because the frequency adjustment provides significant energy savings, especially under a low load. Nevertheless, since the electric drives with a direct supply still prevail in many industries, a number of studies provide comparisons between characteristics of electric motors operating directly from the mains. For instance, Mutize and Wang [14] provides a comparative analysis of the IM of the IE3 energy efficiency class and LSPMSM for fan applications in start-up and steady-state modes. The analysis shows that the steady-state efficiency and power factor of the LSPMSM are significantly higher than that of the IM. However, the analysis was performed at the rated load. The operation of the LSPMSM as part of a pump unit is given in Li et al. [15]. The design of the 2.2 kW IM and LSPMSM and their characteristics in steady-state and transient modes in the case of the rated load and without load are provided in

Kahrisangi et al. [16]. At the rated power mode, a factor of annual cost savings in the case of replacing the IM by the LSPMSM is determined.

One of the main conclusions drawn in References [14–16] is the apparent advantage of LSPMSMs over IMs based on parameters such as efficiency and power factor. However, it should be noted that in said publications, the comparison between IMs and LSPMSMs was performed mainly for the rated modes.

The IE class of an electric motor is determined by its efficiency in the rated mode, in accordance with the IEC 60034-30-1 standard [6]. On the other hand, in heating, ventilation, and air conditioning (HVAC) applications, electric motors run in the rated mode for only a small fraction of the overall operation time.

The present paper discusses operating modes of IMs and LSPMSMs as part of a pump unit with a variable load depending on instantaneous water consumption, for example, in an HVAC application. The paper includes the energy consumption calculations for electric drives at loads different from the rated load of the electric motor, and a comparison of the obtained data in order to assess the energy-saving potential of electric motors of the IE3 and IE4 energy efficiency classes.

The main purpose of the present paper is to determine the criterion for selecting electric motors based on the condition of minimum energy consumption by considering a duty cycle of centrifugal pump units.

2. Characteristics of the Pump Unit and the Motors

The structure of the drive of a pump unit with one electric motor, powered directly from the mains, is shown in Figure 2 [8]. The electric motor is fed directly from the mains and coupled to a centrifugal pump without intermediate mechanical gears.

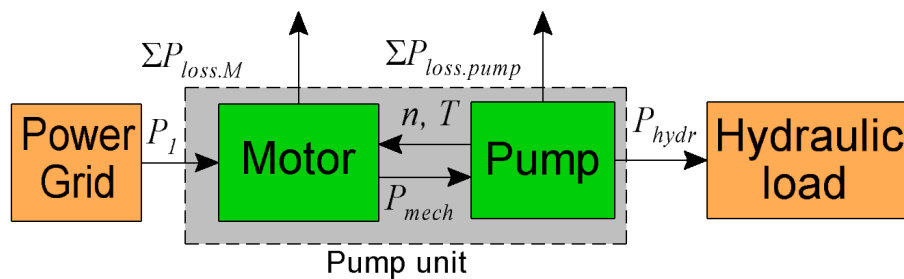


Figure 2. Schematic representation of a single pump unit for fixed-speed operation [8].

The input electrical power from the mains P_1 is converted by the electric motor into the mechanical power (output power) P_{mech} . Power P_{mech} is less than P_1 by the value of the electric motor loss [8]:

$$P_{mech} = P_1 - \Sigma P_{loss.M}, \quad (1)$$

where $\Sigma P_{loss.M}$ is the sum of the motor losses.

The mechanical power P_{mech} of the electric motor is transmitted to the pump, and therefore, in the absence of intermediate mechanical gears, is equal to the input mechanical power of the pump. In the pump, the mechanical power P_{mech} is converted to the hydraulic power P_{hydr} . The difference between P_{mech} and P_{hydr} is the total loss $\Sigma P_{loss.pump}$ in the pump [8]:

$$P_{hydr} = P_{mech} - \Sigma P_{loss.pump}. \quad (2)$$

The hydraulic power is determined using the flow Q and the pump head H_{pump} . The pump head depends on the flow in accordance with the Q - H coefficient of the pump at a given pump rotational speed n .

The required electrical power P_1 depends on the flow Q [8]:

$$P_1 = \rho \cdot g \cdot Q \cdot H_{pump} + \Sigma P_{loss.pump} + \Sigma P_{loss.M}. \quad (3)$$

In order to compare the energy consumption of the electric motors of the pump unit when adjusting flow using a throttle valve, a centrifugal pump NM4 40/25B (manufactured by Calpeda S.p.A., Montorso Vicentino, Vicenza, Italy) with the rated power $P_{RATE} = 2.2$ kW and with rated rotational speed $n = 1450$ rpm [17] was considered. Pump data is shown in Table 1. Q_{BEP} denotes the flow at the best efficient point (BEP), and H_{BEP} denotes the pump head at BEP.

Table 1. Nameplate data of the pump.

Parameter	Type	P_{RATE} (W)	n (rpm)	Q_{BEP} (m ³ /h)	H_{BEP} (m)	Efficiency (%)
Value	NM4 40/25B	2200	1450	19	17.8	60

The calculation was performed for eight different four-pole electric motors with a power of 2.2 kW, namely three LSPMSMs of the IE4 class (Bharat Bijlee SynchroVERT [18], WEG [19], SEW-Eurodrive [20]), two IMs of the IE4 class (Siemens [21] and WEG [22]), and three IMs of the IE3 class (Siemens [21], WEG [23], and ABB [24]). Efficiency data for the electric motors are shown in Table 2.

Table 2. Efficiency of 2.2 kW four-pole electric motors.

m	Type of Motor	Efficiency Class	Efficiency (%) at the Various Loads		
			50%	75%	100%
1	LSPMSM SEW DRU J	IE4	88.0	90.5	91.2
2	LSPMSM SynchroVERT	IE4	88.6	89.4	89.5
3	LSPMSM WEG WQuattro	IE4	86.0	89.0	90.2
4	IM Siemens 1LE1004	IE4	88.3	89.6	89.5
5	IM WEG W22	IE4	88.5	89.5	89.5
6	IM Siemens 1LE1003	IE3	86.4	87.3	86.7
7	IM WEG W21	IE3	86.5	87.0	87.0
8	IM ABB M3BP	IE3	85.1	86.9	86.7

3. Assessment of the Energy Consumption of the Pump Unit

The operation of the pump unit was considered in modes wherein water flow over the duty cycle changed in accordance with the typical characteristic of HVAC applications. A typical pump duty cycle (Figure 3) defined by EC regulations [25] is characterized by four modes. A notable feature of this cycle is that, most of the time, the pump operates at a flow rate much less than the rated value. For example, with the flow of 25% of the rated value, the pump operates for the fraction of time $t_i/t_\Sigma = 44\%$ where t_Σ is the total operation time taken to be equal to 24 h and t_i is the pump operation time in the said mode. Herein, the fraction of the operation time in the rated mode did not exceed 6%. Such a flow-time profile is typical for systems with widely varying demand of flow rate, i.e., for variable flow systems [5].

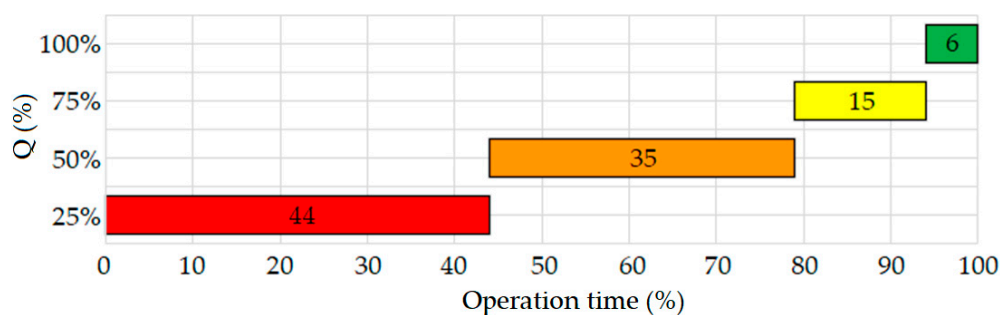


Figure 3. Time dependence of water consumption per cycle.

The electric motor was connected directly to the mains, i.e., motor speed was not adjusted using a frequency converter over the course of the cycle, and the flow Q of the pump was adjusted using a throttle. In this case, the water pressure changed in accordance with the Q - H curve of the pump, and the operating point was the intersection point of the pump characteristic and the hydraulic system characteristic. Figure 4 shows the interpolation results of the Q - H characteristic of the selected pump and the starting points, according to manufacturer data [17].

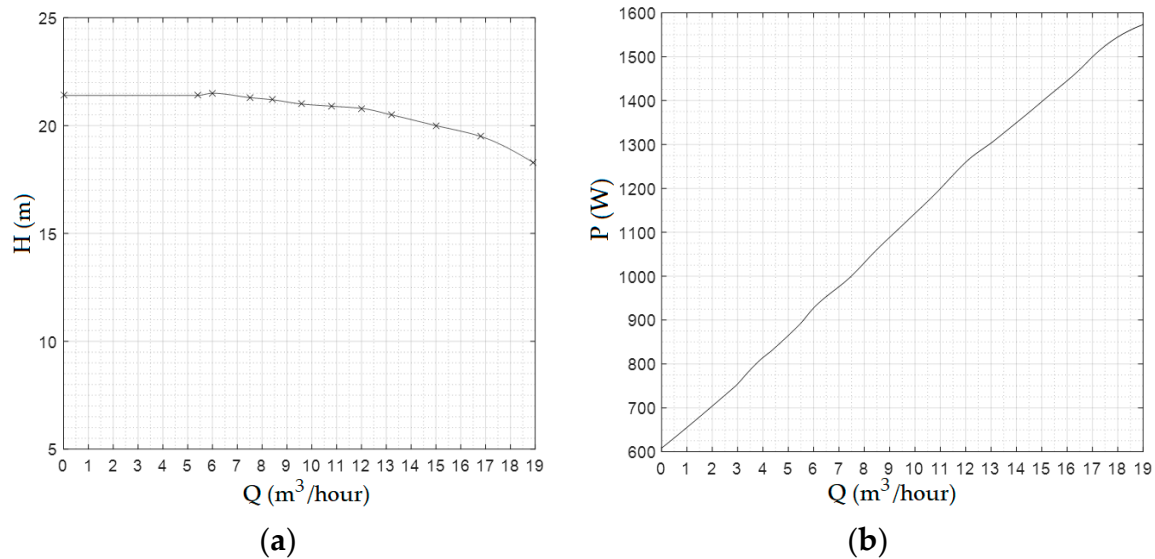


Figure 4. (a) Q - H curve of the pump. (b) Dependence of the pump power on water flow [17].

The mechanical (input) power curve of the pump as a function of flow is reported by the pump manufacturer (Figure 4b). From the curve, the pump power was determined in four operation modes (25%, 50%, 75%, and 100% of the flow). The flow corresponding to 100% was determined based on the pump efficiency curve [17], corresponding to maximum efficiency. Based on the known nameplate data, the efficiencies of the electric motors (Table 2) at the four operation modes of the pump unit were determined using polynomial interpolation of the loss curve $\Sigma P_{loss.M}$ of each electric motor. As seen in Ferreira and De Almeida [26], the correlation between the electric motor loss and load is described well using a second-order polynomial, the coefficients of which can be easily obtained from the efficiencies at three points provided by the electric motors manufacturers.

The obtained efficiency values are provided in Table 3, which also shows the following values for each operating mode: flow, pump head, and mechanical output power of the electric motors as percentages of the rated output. It can be observed that the pump ran in underload modes ($Q < 100\%$) for most of the time. It was assumed that the head varied according to the Q - H curve of the pump (Figure 4a).

The real electric power consumed from the mains in each mode was calculated according to Equation (4):

$$P_{1.i.m} = P_{mech.i.m} / \eta_{M.i.m}, \quad (4)$$

where $\eta_{M.i.m}$ is the efficiency of the m th motor in the i th mode of operation. Calculation results are given in the Table 4.

The daily energy consumption for each electric motor over a full duty cycle of the pump unit in accordance with the corresponding load profile was determined using the Equation (5).

$$E_{d.m} = t_{\Sigma} \cdot \sum_{i=1}^4 \left(P_{1.i.m} \cdot \frac{t_i}{t_{\Sigma}} \right). \quad (5)$$

For the year-round operation of the pump unit, the annual energy consumption was calculated as follows:

$$E_{y,m} = E_{d,m} \cdot 365. \quad (6)$$

Table 3. Interpolated values of efficiency of electric motors.

Mode Number <i>i</i>	1	2	3	4
Operation time (%)	44	35	15	6
Operation time (h/day)	10.56	8.4	3.6	1.44
Q_i (%)	25	50	75	100
Q_i (m ³ /h)	4.75	9.50	14.25	19.00
$H_{pump,i}$ (%)	120	118	113	100
$H_{pump,i}$ (m)	21.4	21.0	20.2	17.8
$P_{mech,i}$ (W)	851	1116	1361	1573
$P_{mech,i}$ (%)	38.7	50.7	61.9	71.5
Efficiency $\eta_{M,i,m}$ (%)				
1. LSPMSM SEW DRU J	85.5	88.1	89.5	90.3
2. LSPMSM SynchroVERT	87.7	88.6	89.1	89.3
3. LSPMSM WEG WQuattro	83.3	86.1	87.8	88.7
4. IM Siemens 1LE1004	86.7	88.4	89.2	89.5
5. IM WEG W22	85.8	88.2	89.3	89.7
6. IM Siemens 1LE1003	84.9	86.5	87.1	87.3
7. IM WEG W21	84.8	86.3	86.9	87.2
8. IM ABB M3BP	82.7	85.2	86.3	86.8

Table 4. Power consumption $P_{1,i,m}$ (W).

Type of Motor	1	2	3	4
1. LSPMSM SEW DRU J	996.2	1266.1	1520.3	1742.3
2. LSPMSM Synchro-VERT	971.3	1258.6	1527.4	1760.8
3. LSPMSM WEG WQuattro	1022.6	1295.2	1550.9	1773.1
4. IM Siemens 1LE1004	982.2	1262.0	1526.3	1757.5
5. IM WEG W22	992.9	1264.8	1524.4	1753.8
6. IM Siemens 1LE1003	1003.1	1289.9	1562.5	1802.5
7. IM WEG W21	1004.4	1293.1	1566.0	1805.0
8. IM ABB M3BP	1029.4	1309.4	1576.4	1812.2

The cost of electricity consumed (in Euro), considering the accepted grid tariffs $GT = 0.1987 \text{ €/kW}\cdot\text{h}$ for non-household consumers [27] for Germany in the second half of 2018, was calculated as follows:

$$C_{y,m} = E_{y,m} \cdot GT. \quad (7)$$

We also assessed the energy consumption during the whole life cycle of the pump system, which is usually 15–20 years [28,29]. We defined the energy cost for the lifespan of $n = 20$ years without taking into account the maintenance costs and the initial cost of the motors since the market cost of the motors depends on many factors and this was beyond of the topic of the present paper. Besides, the pump lifetime cost often consists mostly of the energy cost (>50–60%) [28,29].

The net present value (NPV) of the lifecycle cost was calculated as follows:

$$C_{LCCen,m} = C_{y,m} / (1 + (y - p))^n \quad (8)$$

where y is the interest rate (assumed to be 0.04) and p is the expected annual inflation (assumed to be 0.02) [28,29].

In order to correlate the cost of electricity consumed with using various electric motors in pump units, the differences between the costs of electricity required by the electric motor with the highest

energy consumption (IE3 class motor No. 8 manufactured by ABB, Zürich, Switzerland) and the other seven motors were calculated according to Equation (9). The calculation results according to Equations (4)–(9) are summarized in Tables 4 and 5, and are also shown in Figures 5 and 6.

$$S_{y,m} = C_{y,8} - C_{y,(1 \dots 7)} \quad (9)$$

Table 5. Cost characteristics of the power consumption.

Type of Motor	$E_{d,m}$ (kW·h)	$E_{y,m}$ (kW·h)	$C_{y,m}$ (€)	$C_{LCCen,m}$ (k€)	$S_{y,m}$ (€)
1. LSPMSM SEW DRU J	29.1	10,635	2113.1	34.55	73.8
2. LSPMSM SynchroVERT	28.9	10,535	2093.3	34.23	93.6
3. LSPMSM WEG WQuattro	29.8	10,882	2162.3	35.36	24.6
4. IM Siemens 1LE1004	29.0	10,585	2103.1	34.39	83.8
5. IM WEG W22	29.1	10,630	2112.1	34.54	74.8
6. IM Siemens 1LE1003	29.6	10,822	2150.3	35.16	36.6
7. IM WEG W21	29.7	10,843	2154.4	35.23	32.5
8. IM ABB M3BP	30.2	11,006	2186.9	35.76	0

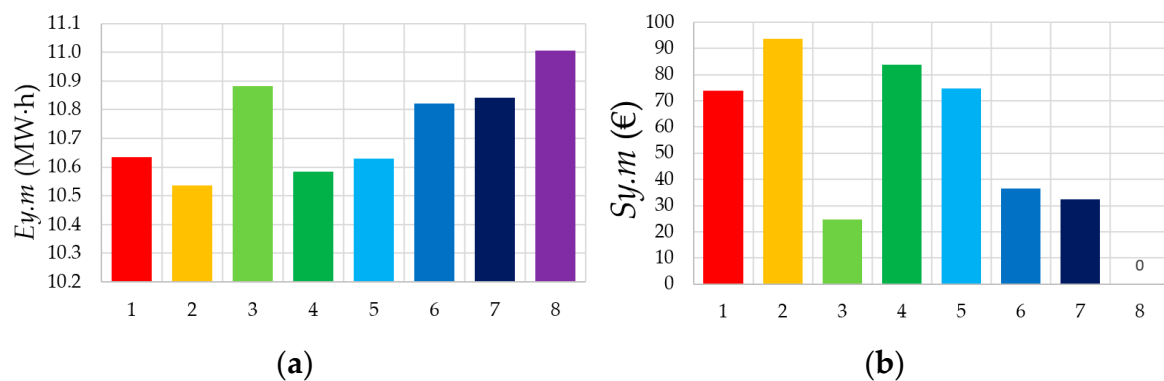


Figure 5. (a) Annual energy consumption. (b) Energy cost savings over electric motor No. 8. 1—LSPMSM IE4 SEW DRU J; 2—LSPMSM IE4 Synchrovert; 3—LSPMSM IE4 Weg WQuattro; 4—IM IE4 Siemens 1LE1004; 5—IM IE4 Weg W22; 6—IM IE3 Siemens 1LE1003; 7—IM IE3 Weg W21; 8—IM IE3 ABB M3BP.

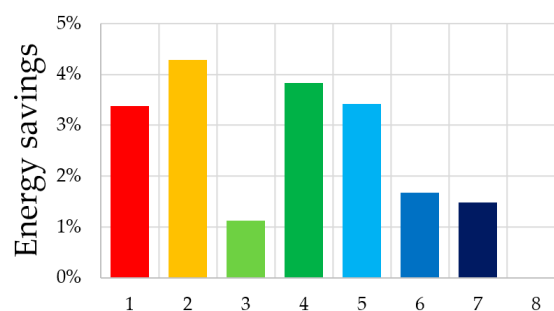


Figure 6. Energy cost savings over electric motor No. 8 (for numbers of the motors see the caption of Figure 5).

Figure 5 shows that the electric motor 3 (LSPMSM of the IE4 the class) consumed more electricity than IMs 6 and 7 of the IE3 class in the considered duty cycle, but less electricity than IM 8 of the IE3 class. Thus, the said IE4 class electric motor provided lower cost savings compared to the IE3 class electric motors 6 and 7. LSPMSMs 1 and 2 had energy consumptions approximately matching those of IMs 4 and 5 of the IE4 class. The lowest energy consumption was exhibited by electric motor 2 (SynchroVERT LSPMSM) and the greatest energy consumption was exhibited by electric motor 8 (IM by ABB).

The results shown in Figure 5a,b are a consequence of the fact that, according to the adopted standard [6], electric motors are classified in accordance with the efficiency in the rated mode (a load of 100%). However, in pump units, electric motors run at 2–4 times lower power than their rated value for a significant part of the time, and as a result, exhibit a reduced efficiency. At the same time, the existing standards do not establish the minimum efficiencies at loads below the rated value for electric motors powered directly from the mains. Thus, the selection of an electric motor based on its IE energy efficiency class will not necessarily result in minimum energy consumption in a number of applications, such as variable flow pumps. It should be noted that for frequency-controlled electric motors, the IEC 60034-30-2 standard [30] establishes the efficiencies in seven load modes different from the rated mode. In the draft version of the IEC 60034-30-2 standard [31], it was proposed that the total efficiency be calculated for frequency-controlled electric motors of pumps and fans (drives with a quadratic torque-speed dependence) as the average efficiency coefficient at reduced speeds and loads. Figure 6 shows the energy cost savings over the worst case of electric motor No. 8 (in %).

Therefore, when selecting an electric motor for a pump unit operating with a variable flow, one should not be guided only by the IE energy-efficiency class and the rated efficiency value; instead, one should calculate the energy consumption depending on the operating conditions or should take into account the energy efficiency index of the pump unit (see Section 4).

It is worth noting that LSPMSMs have a higher cost compared to IMs (especially IE3 class) due to the use of expensive rare-earth magnets in its design. The process of obtaining rare-earth elements from raw ore is associated with significant environmental damage, and in de Lima [32], it is claimed that the production of each ton of rare-earth element material results in the generation of 1–1.4 tons of radioactive waste.

Only a small part of the resulting slush contains rare-earth elements and is subsequently extracted for refinement [32]. There is also a technological dependence on rare-earth element suppliers from China, as more than 95% of the world's rare-earth element mining is controlled by China [33]. In the current situation on the market, the prices of rare-earth elements are unstable and can change several times over several years [34].

Also, the difficulty in starting up LSPMSMs at a significant load moment of inertia severely limits their potential applications. A review of modern papers on LSPMSMs [35–39] shows that the maximum moment of inertia of the load for such electric motors is relatively small and insufficient to start up and reach the rated speed, for example, using a fluid machine with a steel impeller. Such electric motors cannot be started with a large number of typical mechanisms, such as reciprocating compressors, screw compressors, plunger pumps, conveyors, escalators, etc. [35–38].

According to the results of the comparison between LSPMSMs and IMs of classes IE3 and IE4 disclosed in Ferreira et al. [39], LSPMSMs have the highest start-up current peaks, increasing the possibility of nuisance tripping of typical magnetic circuit breakers. This high start-up current can damage contactors, fuses, and other protection devices. Also, using star-delta starters is not recommended or not possible in the case of an LSPMSM. In addition, a voltage decrease and unbalanced supply significantly deteriorate LSPMSM's performances [39].

It can be concluded that, taking into account the aforementioned disadvantages of LSPMSMs, the use of IE4 class IMs in the considered area of application is currently more justified.

4. Assessment of the Energy Efficiency Index of the Pump Unit

The energy efficiency of circulators operating primarily with a variable flow is evaluated in accordance with the EU regulation [25]. The profile indicated in Figure 3 and adopted as a typical pump load profile according to this document [25] is used to perform the calculations in Section 3. Stoffel [8] suggests that the energy efficiency index (EEI) that is already well-established for the assessment of energy efficiency of circulators can be used for other types of pumps and fluid machinery.

Thus, EEI is the most suitable indicator for assessing the energy efficiency of variable flow systems for various purposes, in contrast to the minimum efficiency index (MEI), which is based on

efficiencies in a relatively limited range of operating points (75–110% of the flow) [8] and is defined in the regulation [40].

According to the Europump association approach [41] (p. 12) and to Lang et al. [42], EEI is defined by the formula:

$$EEI = P_{1.avg}/P_{1.ref}, \quad (10)$$

where $P_{1.avg}$ is the average electric power consumed by the pump, which is determined using the following formula [41]:

$$P_{1.avg} = \sum_{i=1}^4 \left[\left(\frac{t_i}{t_{\Sigma}} \right) \cdot P_{1.i} \right]. \quad (11)$$

The denominator in Equation (10), $P_{1.ref}$, is the electric power of the reference system, which according to References [41,42], is determined using Equation (11):

$$P_{1.ref} = P_{hydr.ref}/(\eta_{motor.ref} - \eta_{pump.min.req}), \quad (12)$$

In both formulae, $P_{hydr.ref}$ is the hydraulic power of the reference system, which is defined as the product of flow Q_{BEP} (m³/s) and pump head H_{BEP} (Pa).

In Equation (12), $\eta_{motor.ref}$ is the efficiency of the reference electric motor [6], which was taken to be equal to 86.7% as the corresponding efficiency of a four-pole 2.2 kW electric motor of IE3 energy efficiency class. $\eta_{pump.min.req}$ is the minimum required efficiency of the reference pump at the best efficiency point [40], which depends on the coefficient C determined by the type of pump, the rated rotational speed n of the pump and energy efficiency thereof, the flow Q_{BEP} , and the specific speed n_s , which in turn depends on H_{BEP} and n . A detailed calculation of $\eta_{pump.min.req}$ is not provided in the present document.

Calculation results for Equations (10)–(12) are shown in Table 6.

Table 6. Energy efficiency indexes.

<i>m</i>	Type of Motor	$P_{1.avg}$ (W)	EEI
1	LSPMSM SEW DRU J	1214	0.5786
2	LSPMSM SynchroVERT	1203	0.5732
3	LSPMSM WEG WQuattro	1242	0.5921
4	IM Siemens 1LE1004	1208	0.5759
5	IM WEG W22	1213	0.5784
6	IM Siemens 1LE1003	1235	0.5888
7	IM WEG W21	1238	0.5899
8	IM ABB M3BP	1256	0.5988

By observing the data in Table 6, it is evident that the EEI values for a pump unit with various electric motors corresponds to the patterns made apparent in Figure 5a,b. Therefore, EEI characterizes the energy consumption of a pump unit more objectively than the energy efficiency class (IE) of the electric motor, which depends only on the efficiency in the rated mode.

It should be noted that for circulators subject to the EC regulation [25], since 2005, there has been a voluntary labeling of products by members of the Europump Association using the A–G letter grade for the energy efficiency class. The introduction of such labeling for industrial pump units may also be a consideration.

5. Conclusions

The present paper provides a comparative analysis of the energy consumption of electric motors of various types (LSPMSMs and IMs) and energy efficiency classes (IE3 and IE4) used as part of a 2.2 kW variable-speed pump unit with throttle control. The approach used for comparing the energy characteristics of electric motors is described, including the calculation of energy consumption by a

pump unit in a typical duty cycle containing various hydraulic load values. Electric power values, energy consumption, and cost savings for eight electric motors were calculated.

According to the results of the calculation carried out using the disclosed method and performed on the basis of the nameplate data of electric motors and pumps, it was shown that the use of an electric motor with a higher efficiency at the rated load (high energy efficiency class, according to IEC 60034-30-1 standard [6]) does not always provide a lower energy consumption in pump units with variable fluid flow. The method further shows that the considered IE4 class LSPMSMs may not provide significant advantages over IE4 class IMs, and sometimes even over IE3 class IMs when they are used in variable flow fixed-speed applications.

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